# DEVELOPMENT OF HIGHWAY HORIZONTAL ALIGNMENT ANALYSIS ALGORITHM APPLICABLE TO THE ROAD SAFETY SURVEY AND ANALYSIS VEHICLE, ROSSAV 

Dukgeun YUN
Researcher
Highway Research Department
Korea Institute of Construction Technology 2311, Daehwa-Dong, Ilsan-Gu, Goyang-Si, Gyeonggi-Do, 411-712, Korea
Fax : +81-31-9100-746
E-mail : dkyun@kict.re.kr

Junggon SUNG<br>Research Fellow<br>Highway Research Department<br>Korea Institute of Construction Technology 2311, Daehwa-Dong, Ilsan-Gu, Goyang-Si, Gyeonggi-Do, 411-712, Korea<br>Fax : +81-31-9100-746<br>E-mail : jgsung@kict.re.kr


#### Abstract

In this research, the horizontal alignment analysis algorithm was developed which can recognize the highway sections whether they are tangent sections or curve sections using the real world coordinate data. The proposed algorithm for horizontal curve analysis includes the identification of beginning and ending points of horizontal curves for the circular and transition curves, the parameter of clothoid, radius of circular curve, and length of circular and transition curves. The calculated coordinates for the beginning of curve, beginning of tangency, values for the radius, length of curve, clothoid parameter, and central angle show almost similar to the real world coordinates and real world values. The analysis algorithm of horizontal curves expects to be used as a basis of automatic procedure which can identify the highway deficient sections along the highway route and analyze highway safety in terms of quantitative measures.


Key Words: Horizontal Curve, Highway Safety, GPS, INS, CCD

## 1. INTRODUCTION

In order to evaluate highway safety, it is essential to have highway geometric information such as horizontal alignments, vertical alignments, and cross section information. Most analyses of geometric alignments have been done using the highway drawings. In many cases, however highway drawings are not always available and they are inconvenient to be used for the analysis of a long highway section along the route since the highway drawings are usually made for a certain short distance such as $500 \mathrm{~m}, 800 \mathrm{~m}$, and so on.
For these reasons, the RoSSAV(Road Safety Survey and Analysis Vehicle) has been developed in order to collect highway geometric information and to analyze the highway sections along the highway route. Multiple sensors were installed to collect highway geometric information such as GPS(Global Positioning System), IMU(Inertial Measurement Unit), DMI(Distance Measuring Instrument) and CCD cameras to acquire real world highway coordinates and attitude data. More sensors like laser scanning sensor are considered to be installed to get more realistic cross sectional data and roadside environment data. Figure 1 shows the RoSSAV.(Yun et al., 2004)
The data from the RoSSAV include real-world position data and orientation data. Since the RoSSAV records simple numerical data, the real world coordinates, which represent GPS antenna location, the coordinate data need to be interpreted into the highway geometric data. In order to use these data to analyze the highway horizontal alignments, first of all, the
horizontal alignment analysis algorithm was developed. The purpose of this study is to develop the highway horizontal alignment analysis algorithm which can be applicable directly using the position and orientation data from the RoSSAV in the near future. The identification algorithm includes the identification logic whether the section calculated from the coordinates is tangent or curve section. Once the section is determined as a curve section then it should be determined whether this section is a simple circular curve, a transition curve, or a compound curve. In this study, only simple circular curve and clothoid curve were taken into consideration for the curve section analysis. An identification analysis algorithm for the circular curve and clothoid curve has been developed. The values of highway alignment elements needed for the curve section analysis are the radius of circular curve, length of curve, center point of curve, central angle, and clothoid parameter.


Figure 1. Road Safety Survey and Analysis Vehicle (RoSSAV)

## 2. HORIZONTAL ALIGNMENT ANALYSIS ALGORITHM

The horizontal alignment analysis algorithm from the coordinates is shown in Figure 2. (Yun et al, 2004)


Figure 2. Horizontal Curve Analysis Algorithm

### 2.1 Analysis of Horizontal Curves

The horizontal alignments are analyzed using the real world highway coordinates. The procedure of horizontal curve analysis from the coordinates is as follows:

1) Identification of tangent section and curve section including beginning and ending points of curve
2) Identification of simple curve and clothoid curve
3) Analysis of geometric information for simple curve and clothoid

## 1) Analysis of beginning and ending points of horizontal curve

The procedure for determining the tangent and curve sections is made by gradient changing point from the comparison of gradients using two consecutive coordinates. If the gradient becomes changed from the constant gradient, it can be identified that highway section is changed from tangent section to curve section, and if the gradient becomes constant from the changing gradient, then it can be identified that highway section is changed from the curve section to tangent section.


Figure 3. Change of Gradient for Tangent and Curve Section
Figure 3 shows the change of gradient in tangent and curve section. The analysis algorithm for tangent and curve section is as follows.
(a) Calculation of Gradient from the two consecutive coordinates

The gradient for the two consecutive coordinates is calculated using Equation 1.
$\delta_{2,1}=\frac{\left(y_{2}-y_{1}\right)}{\left(x_{2}-x_{1}\right)}, \delta_{3,2}=\frac{\left(y_{3}-y_{2}\right)}{\left(x_{3}-x_{2}\right)}, \cdots \cdots, \delta_{i, i-1}=\frac{\left(y_{i}-y_{i-1}\right)}{\left(x_{i}-x_{i-1}\right)} \quad<$ Equation 1>
where, $\delta_{i, i-1}:\left(x_{i-1}, y_{i-1}\right),\left(x_{i}, y_{i}\right):$ Gradient using two consecutive coordinates
(b) Coordinates (BC and BT) that changes gradient

When two consecutive gradients are compared,
If gradient $=\left\{\begin{array}{c}\text { constant and become changed at } \delta_{i, i-1} \\ \rightarrow\left(x_{i-1}, y_{i-1}\right) \text { can be beginning curve(BC) } \\ \text { changing and become constant at } \delta_{i, i-1} \\ \rightarrow\left(x_{i-1}, y_{i-1}\right) \text { can be ending curve(BC) }\end{array}\right.$


Figure 4. Tangent and Curve Section

## 2) Identification of Clothoid Curve and Simple Curve

For this study, only simple curve and clothoid curve are considered. Simple curve and Clothoid curve have their own equations and geometric characteristics. Therefore it should be analyzed separately. Once the gradient analysis shows curve section, it is assumed as simple curve. If the simple curve equation is not satisfied, then the curve section becomes clothoid section.

## (a) Simple Curve Equation

In order to distinguish clothoid and simple curves by the gradient analysis, once the curve section begins, it is assumed that all the coordinates are satisfied by the simple curve equation. First, all curve sections are assumed as simple curves and all coordinates within curve section satisfy with the simple curve equation as shown in Figure 5.


Where $\left(x_{i}, y_{i}\right),\left(x_{i+1}, y_{i+1}\right), i:$ Coordinate within Tangent Section
$\left(\mathrm{x}_{\mathrm{c}}, \mathrm{y}_{\mathrm{c}}\right),\left(\mathrm{x}_{\mathrm{c}+1}, \mathrm{y}_{\mathrm{c}+1}\right), \mathrm{i}:$ Coordinate within Circular Section
Figure 5. Coordinates within Tangent and Curve Section

Equation 2 shows simple curve equation using the coordinates.

$$
\begin{array}{ll}
\left(x-x_{M}\right)^{2}+\left(y-y_{M}\right)^{2}=R^{2} & <\text { Equation } 2> \\
\text { where, } x_{M}, y_{M}: \text { Center of Circle, }, & \mathrm{R}: \text { Radius of Circle }
\end{array}
$$

## (b) Three Consecutive Coordinates on the Curve Section

Using three consecutive coordinates $\left(x_{C}, y_{C}\right),\left(x_{C+1}, y_{C+1}\right),\left(x_{C+2}, y_{C+2}\right)$, the center of curve and radius of curve can be calculated by Equation 3, 4 and 5.

$$
\begin{array}{ll}
x_{M}=\frac{\left(x_{c+2}^{2}+y_{c+2}^{2}\right)-\left(x_{c}^{2}+y_{c}^{2}\right)+\left\{\frac{\left.\left(x_{c+1}^{2}+y_{c+1}^{2}\right)-x_{2}^{2}+y_{2}^{2}\right\}}{\left(y_{c+1}+y_{c}\right)}\right\}\left(y_{c}-y_{c+2}\right)}{2\left\{\left(x_{c+2}-x_{c}\right)+\frac{\left(x_{c}-x_{c+1}\right)}{\left(y_{c+1}-y_{c}\right)}\left(y_{c+2}-y_{c}\right)\right\}} & <\text { Equation3>} \\
y_{M}=\frac{\left(x_{c+1}^{2}+y_{c+1}^{2}\right)-\left(x_{c}^{2}+y_{c}^{2}\right)+2 x_{M}\left(x_{c}-x_{c+1}\right)}{2\left(y_{c+1}-y_{c}\right)} & \\
R=\sqrt{\left(x_{c}-x_{M}\right)^{2}+\left(y_{c}-y_{M}\right)^{2}} & <\text { Equation 4> } \\
& <\text { Equation 5> }
\end{array}
$$

## (c) Identification of Clothoid and Simple Curve

In the previous step, the algorithm assumes that the horizontal alignments are composed of tangent and simple curve sections and all coordinates within the curve section satisfy the simple circle equation. In order to satisfy this assumption, any three consecutive coordinates should satisfy the constant numbers for the center of circle ( $x_{M}, y_{M}$ ) and radius of circle R from the Equation 3 through Equation 5. If the calculated number of $x_{M}, y_{M}$, and R are not constant from three consecutive coordinates, this curve does not satisfy the simple curve equation and will be considered as a clothoid curve. If the calculated numbers ( $x_{M}, y_{M}, \mathrm{R}$ ) are not constant, these coordinates are on the clothoid curve.

Therefore,

$$
\begin{array}{ll}
\frac{\left(x_{M: C \sim C+2}\right)}{\left(x_{M: C+1 \sim C+3}\right)} \times \frac{\left(y_{M: C \sim C+2}\right)}{\left(y_{M: C+1 \sim C+3}\right)} \times \frac{R_{C \sim C+2}}{R_{C+1 \sim+3}}=1 & \\
\quad \rightarrow\left(x_{C}, y_{C}\right) \sim\left(x_{C+3}, y_{C+3}\right) \quad \text { are on the simple curve } & \text { <Equation 6> } \\
\frac{\left(x_{M: C \sim C+2}\right)}{\left(x_{M: C+1 \sim C+3}\right)} \times \frac{\left(y_{M: C \sim+2}\right)}{\left(y_{M: C+1 \sim C+3}\right)} \times \frac{R_{C \sim C+2}}{R_{C+1 \sim+3}} \neq 1 & \\
\quad \rightarrow\left(x_{C}, y_{C}\right) \operatorname{cr}\left(x_{C+3}, y_{C+3}\right) & \text { are on the clothoid curve }
\end{array} \quad \text { <Equation 7> }
$$

where, $x_{M: C \sim C+2}, y_{M: C \sim C+2}, R_{M: C \sim C+2}$ are $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}, \mathrm{R}$ three consecutive coordinates on the $\left(x_{C}, y_{C}\right),\left(x_{C+1}, y_{C+1}\right),\left(x_{C+2}, y_{C+2}\right)$ curve section

If three coordinates $\left(x_{C}, y_{C}\right),\left(x_{C+1}, y_{C+1}\right),\left(x_{C+2}, y_{C+2}\right)$ all satisfy the simple curve, Equation 6 is satisfied. If any of these three coordinates is not included, Equation 7 will be resulted.


Figure 6. Coordinates within Simple Curve and Clothoid Curve

## 3) Geometric Information of Simple Curve

Identify simple curve and clothoid curve using Equation 6 and 7, and select coordinates on the simple curve. The center of circle and radius of circle are calculated by the Equation 3 through Equation 5. The length of simple curve and angle $\theta$ can be calculated as follows. (Hickerson, T., 1964)


Figure 7. Simple Curve Geometry
a) Calculation of Central Angle $\boldsymbol{\Theta}$

The coordinates of beginning of curve $(\mathrm{BC})$ and end of curve(EC) are $\left(x_{B C}, y_{B C}\right)\left(x_{B C}, y_{B C}\right)$. The length of chord L which connects the beginning of curve and the end of curve can be calculated as follows.

$$
L=\sqrt{\left(x_{B C}-x_{E C}\right)^{2}+\left(y_{B C}-y_{E C}\right)^{2}}
$$

<Equation 8>

The central angle ecan be calculated using Equation 9.

$$
\begin{aligned}
& \sin \left(\frac{\theta}{2}\right)=\frac{L}{2 R} \\
& \theta=2 \sin ^{-1}\left(\frac{L}{2 R}\right)
\end{aligned}
$$

<Equation 9>

## b) Calculation of the Length of Circular Curve $S$

The length of circular curve $S$ can be calculated by Equation 10 using the radius $R$ and $\theta$ from the Equation 8 through Equation 9, and L from the Equation 8.

$$
\begin{aligned}
& S=R \cdot \theta \\
& =R \cdot 2 \sin ^{-1}\left(\frac{L}{2 R}\right) \\
& =R \cdot 2 \sin ^{-1}\left(\frac{\sqrt{\left(x_{B C}-x_{E C}\right)^{2}+\left(y_{B C}-y_{E C}\right)^{2}}}{2 R}\right)
\end{aligned}
$$

## 4) Geometric Information of Clothoid Curve

In this study, only clothoid curve is assumed as transition curve. If a tangent section connects directly to a circular curve, the radius of R abruptly changes from $\infty$ to constant value and that makes a driver feel uncomfortable. The transition curve can improve smooth driving for the curve section by changing radius of curve from $\infty$ to constant value smoothly. Therefore the radii of curve are continuously reduced and make the length of clothoid L from the beginning of curve and radius R be inversely proportional.(TAC, 1999)

$$
L \times R=C \text { (constant }) \quad<\text { Equation 11> }
$$

where L : length of clothoid curve (m)
R : Radius(m)
C: Constant $\left(\mathrm{m}^{2}\right)$
As shown in Figure 8, let two points on the clothoid $\mathrm{P}_{1}, \mathrm{P}_{2}$, and the length of clothoid curve from the beginning point of curve BTC as $\mathrm{P}_{1}, \mathrm{P}_{2}$, then

$$
L_{1} \times R_{1}=L_{2} \times R_{2}=C \quad<\text { Equation 12 }>
$$

The unit of $C$ becomes $\mathrm{m}^{2}$. If replace $\mathrm{C}=\mathrm{A}^{2}$ for the convenience, the equation becomes Equation 13.
$L \times R=A^{2}$
<Equation 13>
A : parameter of clothoid
The radius at the connecting point of the clothoid curve and circular curve becomes R . The clothoid parameter A can be calculated by Equation 13 using the length of clothoid L and radius of curve $R$. The length of clothoid curve $L$ from the beginning point BTC to the beginning point of circular curve BC can be calculated using the coordinates.


Figure 8. Geometry of Clothoid Curve

## 3. EXAMPLE OF HORIZONTAL ALIGNMENT ANALYSIS

In order to check the logic from the algorithm, two tests were performed using real world highway CAD drawings in order to apply the algorithm to the RoSSAV,

1) tangent section-clothoid curve section-simple curve section highway alignments and
2) tangent section-simple curve section 1 -simple curve section 2 - tangent section highway alignments. The developed horizontal alignment analysis algorithm and CAD based drawings were compared by checking the coordinates.

### 3.1 Simple Horizontal Alignment Case.

Figure 9 shows as an example of highway alignment which composed of 'tangent section(T) -clothoid curve section(BTC)-simple curve(BC)-clothoid curve section(EC) -tangent section(ETC)'.


Figure 9. Transition Curve and Simple Circular Curves
The $\mathrm{X}, \mathrm{Y}$ coordinates for every 1 m from the real world highway horizontal alignment CAD drawing are drawn and the coordinates are shown in Figure 10.


Figure 10. Coordinates from the Horizontal Alignment CAD Drawing

The results of analysis for the tangent section, transition curve section and simple circular curve sections are shown in Table 1.

Table 1. Coordinates and Horizontal Alignment Analysis

| No | X | y | gradient | $\mathrm{x}_{\mathrm{M}}$ | $\mathrm{y}_{\mathrm{M}}$ | R (m) | section |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.314652 | $3.70 \mathrm{E}-02$ |  |  |  |  | Tangent Section <br> - constant gradient |
| 2 | 1.307797 | 0.153924 | 0.117697 | $-2.5 \mathrm{E}+13$ | $2.1 \mathrm{E}+14$ | $2.12 \mathrm{E}+14$ |  |
| 3 | 2.300942 | 0.270814 | 0.117697 | $2.45 \mathrm{E}+13$ | $-2.1 \mathrm{E}+14$ | $2.09 \mathrm{E}+14$ |  |
| 4 | 3.294086 | 0.387705 | 0.117697 | $-3 \mathrm{E}+13$ | $2.52 \mathrm{E}+14$ | $2.53 \mathrm{E}+14$ |  |
| 5 | 4.287231 | 0.504595 | 0.117697 | $4.5 \mathrm{E}+14$ | $-3.8 \mathrm{E}+15$ | $3.85 \mathrm{E}+15$ |  |
| ...... omitted...... |  |  |  |  |  |  |  |
| 165 | 163.1904 | 19.20706 | 0.117697 | $6.68 \mathrm{E}+12$ | $-5.7 \mathrm{E}+13$ | $5.72 \mathrm{E}+13$ |  |
| 166 | 164.1835 | 19.32395 | 0.117697 | -5607.91 | 49056.93 | 49376.15 |  |
| 167 | 165.1767 | 19.44084 | 0.117697 | -5680.96 | 49686.15 | 50009.59 | Clothoid Curve(BTC) |
| 168 | 166.1698 | 19.55775 | 0.117718 | -5891.63 | 51475.62 | 51811.42 | Clothoid Curve <br> -changing gradient <br> - changing $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}, \mathrm{R}$ |
| 169 | 167.163 | 19.67468 | 0.117738 | -9101.98 | 78742.22 | 79266.36 |  |
| 170 | 168.1561 | 19.79163 | 0.117758 | -4477.76 | 39468.74 | 39721.58 |  |
| 171 | 169.1492 | 19.90859 | 0.11777 | -3725.51 | 33085.52 | 33294.19 |  |
| 172 | 170.1424 | 20.02558 | 0.117796 | -3447.41 | 30726.1 | 30918.43 |  |
| 173 | 171.1355 | 20.1426 | 0.117826 | -2648.45 | 23945.86 | 24091.29 |  |
| 174 | 172.1286 | 20.25965 | 0.117859 | -2176.93 | 19947.06 | 20064.78 |  |
| $\ldots .$. omitted $\ldots . .$. |  |  |  |  |  |  |  |
| 477 | 465.7158 | 89.00982 | 0.479651 | 175.8977 | 692.0805 | 669.0955 |  |
| 478 | 466.6167 | 89.44385 | 0.481766 | 123.2795 | 800.9557 | 790.0187 |  |
| 479 | 467.517 | 89.87922 | 0.48361 | 201.3464 | 639.1138 | 610.3322 |  |
| 480 | 468.4167 | 90.31573 | 0.485173 | 338.2809 | 357.3956 | 297.0976 |  |
| 481 | 469.3157 | 90.75371 | 0.487197 | 360.4801 | 313.0031 | 247.4671 | mple Circular Curve (BC) |
| 482 | 470.2132 | 91.1947 | 0.491354 | 266.139 | 505.3908 | 461.7409 | Simple Circular Curve |
| 483 | 471.1089 | 91.63932 | 0.496374 | 266.139 | 503.4492 | 460 |  |
| 484 | 472.0036 | 92.08588 | 0.499086 | 266.139 | 503.4492 | 460 |  |
| 485 | 472.8974 | 92.53438 | 0.501805 | 266.139 | 503.4492 | 460 |  |
| 486 | 473.7902 | 92.98482 | 0.504529 | 266.139 | 503.4492 | 460 |  |
| $\ldots .$. omitted ..... |  |  |  |  |  |  | -changing gradient -constant $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}, \mathrm{R}$ |
| 724 | 649.6329 | 249.4168 | 1.506068 | 266.139 | 503.4492 | 460 |  |
| 725 | 650.1843 | 250.2511 | 1.513196 | 266.139 | 503.4492 | 460 |  |
| 726 | 650.7338 | 251.0866 | 1.520371 | 266.139 | 503.4492 | 460 |  |
| 727 | 651.2815 | 251.9232 | 1.527594 | 266.139 | 503.4492 | 460 |  |
| 728 | 651.8274 | 252.7611 | 1.534865 | 491.7225 | 356.4764 | 190.7628 |  |
| 729 | 652.3714 | 253.6001 | 1.542185 | 229.5924 | 527.1472 | 503.5575 | Simple Circular Curve (EC) |
| 730 | 652.9111 | 254.442 | 1.560003 | -58.2378 | 709.7119 | 844.3953 | Clothoid Curve -changing gradient <br> - changing $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}, \mathrm{R}$ |
| 731 | 653.4491 | 255.285 | 1.566857 | 152.7725 | 574.2338 | 593.6374 |  |
| 732 | 653.9861 | 256.1286 | 1.570959 | 123.3288 | 593.3279 | 628.7293 |  |
| ..... omitted ..... |  |  |  |  |  |  |  |
| 1042 | 758.1576 | 546.4612 | 4.224667 | -28957.9 | 7579.887 | 30537.07 |  |
| 1043 | 758.3879 | 547.4343 | 4.224876 | -129017 | 31263.84 | 133360.7 |  |
| 1044 | 758.6182 | 548.4075 | 4.225493 | $9.52 \mathrm{E}+11$ | $-2.3 \mathrm{E}+11$ | $9.79 \mathrm{E}+11$ | Clothoid Curve (ETC) |
| 1045 | 758.8485 | 549.3806 | 4.225634 | $-9.8 \mathrm{E}+11$ | $2.31 \mathrm{E}+11$ | $1 \mathrm{E}+12$ | Tangent Section - constant gradient |

The comparison of coordinates from the algorithm and coordinates of highway CAD drawing are summarized in Table 2.

Table 2. Coordinates from the Algorithm and Coordinates from CAD Drawing

| Section |  | Calculated Coordinates | CAD Coordinates |
| :---: | :---: | :---: | :---: |
| Beginning point of Clothoid Curve(BTC) | x | 165.1767 | 165.6701 |
|  | y | 19.44084 | 19.4989 |
| Beginning Point of Simple Circular Curve (BC) | x | 469.3157 | 469.6823 |
|  | y | 90.75371 | 90.9323 |
| End Point of Simple Circular Curve (EC) | x | 652.3714 | 652.5209 |
|  | y | 253.6001 | 253.8314 |
| End Point of Clothoid Curve(ETC) | x | 758.6182 | 758.4308 |
|  | y | 548.4075 | 547.6157 |

The clothoid parameter A, radius of curve R, length of simple circular curve $S$, central angle $\Theta$ are shown in Table 3.

Table 3. Comparison of R, S, $\Theta, A$

| Design Elements | Calculated | CAD | Equation |
| :---: | :---: | :---: | :---: |
| Radius of Curve(R) | 460 m | 460 m | <Equation 5> |
| Central Angle( $\Theta$ ) | $30.6^{\circ}$ | $30^{\circ}$ | <Equation 9> |
| Length of Simple Circular <br> Curve(S) | 246 m | 247.9 m | <Equation 10> |
| Clothoid Parameter(A) | 380 m | 380 m | $<$ Equation 13> |

When Table 2 and 3 are compared, the calculated coordinates and values from the algorithm are not different with those of highway CAD drawing.

### 3.2 Reverse Horizontal Curve Case

In order to test the analysis algorithm, reverse curve case was analyzed which are shown in Figure 11. The highway alignments are composed of 'tangent section-simple circular curve 1simple circular curve 2 - simple circular curve 3 - tangent section. The developed algorithm was applied.


Figure 11. Reverse Curve Case
For the reverse curve case, the calculation of the center of curve ( $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}$ ) from the consecutive three points and radius R is shown in Figure 12. For the circled points, the center of curve and radius do not have constant values, and after the certain section, the center of curve and radius has constant values.


Figure 12. Change of Center of Curve and $R$ for the Reverse Curves
For the reverse curve analysis, tangent section, simple circular curve 1 , simple circular curve 2, and simple circular curve 3 were analyzed and summarized in Table 4. Table 4 shows that the gradient is changing at the point of curve, for the simple circular curve 1 , the center of curve ( $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}$ ) and radius of curve R are constant for the simple circular curve 2 and 3. As shown in Figure 8, if gradient is changing and the center of curve ( $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}$ ) and the radius of curve R are changing for a relatively long section, the curve is assumed as transition curve. Then the analysis of transition curve is performed. However, if the gradient is changing and the center of curve $\left(\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}\right)$ and the radius of curve R are changing only for
short section, then it is assumed that this section is the part of the reverse curve.
Table 4. Coordinates and Horizontal Alignment Analysis for the Reverse Curve

| No | x | y | gradient | $\mathrm{x}_{\mathrm{M}}$ | $\mathrm{y}_{\mathrm{M}}$ | R | section |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 473.79556 | 196.70587 |  |  |  |  | Tangent Section <br> - constant gradient |
| 2 | 474.65870 | 196.20091 | -0.585034 |  |  |  |  |
| 3 | 475.52184 | 195.69594 | -0.585034 | $-9.259 \mathrm{E}+11$ | $-6.141 \mathrm{E}+02$ | $9.26 \mathrm{E}+11$ |  |
| 4 | 476.38498 | 195.19098 | -0.585034 | $1.759 \mathrm{E}+13$ | $-1.583 \mathrm{E}+12$ | $1.77 \mathrm{E}+13$ |  |
| 5 | 477.24812 | 194.68601 | -0.585034 | $2.056 \mathrm{E}+13$ | $3.007 \mathrm{E}+13$ | $3.64 \mathrm{E}+13$ |  |
| 6 | 478.11126 | 194.18105 | -0.585034 | $-1.292 \mathrm{E}+12$ | $3.515 \mathrm{E}+13$ | $3.52 \mathrm{E}+13-$ |  |
| 7 | 478.97440 | 193.67608 | -0.585034 | $1.495 \mathrm{E}+12$ | $-2.208 \mathrm{E}+12$ | $2.67 \mathrm{E}+12$ |  |
| ...... omitted..... |  |  |  |  |  |  |  |
| 246 | 685.26473 | 72.98931 | -0.585034 | $1.352 \mathrm{E}+12$ | $6.028 \mathrm{E}+12$ | $6.18 \mathrm{E}+12$ |  |
| 247 | 686.12787 | 72.48434 | -0.585034 | $-1.100 \mathrm{E}+12$ | $2.312 \mathrm{E}+12$ | $2.56 \mathrm{E}+12$ |  |
| 248 | 686.99101 | 71.97938 | -0.585034 | $-1.118 \mathrm{E}+13$ | $-1.879 \mathrm{E}+12$ | $1.13 \mathrm{E}+13 \mathrm{C}$ | rcular Curve 1 |
| 249 | 687.85428 | 71.47463 | -0.584696 | $2.693 \mathrm{E}+03$ | $-1.910 \mathrm{E}+13$ | $1.91 \mathrm{E}+13$ | Circular Curve 1 -changing gradient - constant $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}, \mathrm{R}$ |
| 250 | 688.71843 | 70.97140 | -0.582348 | $9.756 \mathrm{E}+02$ | $3.501 \mathrm{E}+03$ | 3442.385 |  |
| 251 | 689.58358 | 70.46989 | -0.579672 | $9.399 \mathrm{E}+02$ | $5.645 \mathrm{E}+02$ | 553.867 |  |
| 252 | 690.44974 | 69.97012 | -0.577004 | $9.399 \mathrm{E}+02$ | $5.033 \mathrm{E}+02$ | 500 |  |
| 253 | 691.31689 | 69.47207 | -0.574341 | $9.399 \mathrm{E}+02$ | $5.033 \mathrm{E}+02$ | 500 |  |
| 254 | 692.18504 | 68.97577 | -0.571684 | $9.399 \mathrm{E}+02$ | $5.033 \mathrm{E}+02$ | 500 |  |
| $\ldots .$. omitted ..... |  |  |  |  |  |  |  |
| 882 | 1276.18342 | 133.27576 | 0.906986 | $9.399 \mathrm{E}+02$ | $5.033 \mathrm{E}+02$ | 500 |  |
| 883 | 1276.92279 | 133.94906 | 0.910638 | $9.399 \mathrm{E}+02$ | $5.033 \mathrm{E}+02$ | 500 |  |
| 884 | 1277.66081 | 134.62384 | 0.914303 | $9.399 \mathrm{E}+02$ | $5.033 \mathrm{E}+02$ | 500 |  |
| 885 | 1278.39748 | 135.30009 | 0.917982 | $9.399 \mathrm{E}+02$ | $5.033 \mathrm{E}+02$ | 500 | Circular Curve 2 |
| 886 | 1279.13320 | 135.97738 | 0.920582 | $7.981 \mathrm{E}+02$ | $5.033 \mathrm{E}+02$ | 605.2192 | Circular Curve 2 <br> -changing gradient <br> - constant $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}, \mathrm{R}$ |
| 887 | 1279.86968 | 136.65383 | 0.918485 | $1.875 \mathrm{E}+03$ | $6.577 \mathrm{E}+02$ | 790.8847 |  |
| 888 | 1280.60714 | 137.32923 | 0.915854 | $1.753 \mathrm{E}+03$ | $-5.118 \mathrm{E}+02$ | 802.8638 |  |
| 889 | 1281.34555 | 138.00357 | 0.913231 | $1.753 \mathrm{E}+03$ | $-3.792 \mathrm{E}+02$ | 700 |  |
| 890 | 1282.08493 | 138.67686 | 0.910614 | $1.753 \mathrm{E}+03$ | $-3.792 \mathrm{E}+02$ | 700 |  |
| 891 | 1282.82527 | 139.34909 | 0.908004 | $1.753 \mathrm{E}+03$ | $-3.792 \mathrm{E}+02$ | 700 |  |
| ..... omitted |  |  |  |  |  |  |  |
| 1583 | 1927.60110 | 298.65440 | -0.256782 | $1.753 \mathrm{E}+03$ | $-3.792 \mathrm{E}+02$ | 700 |  |
| 1584 | 1928.56932 | 298.40430 | -0.258305 | $1.753 \mathrm{E}+03$ | $-3.792 \mathrm{E}+02$ | 700 |  |
| 1585 | 1929.53718 | 298.15282 | -0.259830 | $1.753 \mathrm{E}+03$ | $-3.792 \mathrm{E}+02$ | 700 | Circular Curve 3 |
| 1586 | 1930.50482 | 297.90048 | -0.260786 | $1.648 \mathrm{E}+03$ | $-3.792 \mathrm{E}+02$ | 733.6482 | Circular Curve 3 <br> -changing gradient <br> - constant $\mathrm{x}_{\mathrm{M}}, \mathrm{y}_{\mathrm{M}}, \mathrm{R}$ |
| 1587 | 1931.47281 | 297.64949 | -0.259288 | $2.110 \mathrm{E}+03$ | $-7.829 \mathrm{E}+02$ | 1095.221 |  |
| 1588 | 1932.44122 | 297.40011 | -0.257510 | $2.082 \mathrm{E}+03$ | $9.878 \mathrm{E}+02$ | 706.3429 |  |
| 1589 | 1933.41004 | 297.15235 | -0.255734 | $2.082 \mathrm{E}+03$ | $8.786 \mathrm{E}+02$ | 600 |  |
| 1590 | 1934.37927 | 296.90621 | -0.253959 | $2.082 \mathrm{E}+03$ | $8.786 \mathrm{E}+02$ | 600 |  |
| 1591 | 1935.34891 | 296.66168 | -0.252185 | $2.082 \mathrm{E}+03$ | $8.786 \mathrm{E}+02$ | 600 |  |
| $\ldots .$. . omitted ..... |  |  |  |  |  |  |  |
| 2384 | 2609.46865 | 593.37529 | 1.847295 | $2.082 \mathrm{E}+03$ | $8.786 \mathrm{E}+02$ | 600 |  |
| 2385 | 2609.94323 | 594.25550 | 1.854672 | $2.082 \mathrm{E}+03$ | $8.786 \mathrm{E}+02$ | 600 |  |
| 2386 | 2610.41661 | 595.13636 | 1.860812 | $1.972 \mathrm{E}+03$ | $8.786 \mathrm{E}+02$ | 698.8542 | Tangent Section |
| 2387 | 2610.88986 | 596.01729 | 1.861446 | $-3.589 \mathrm{E}+03$ | $9.379 \mathrm{E}+02$ | 6209.69 | Tangent Section constant gradient |
| 2388 | 2611.36311 | 596.89822 | 1.861446 | $-9.007 \mathrm{E}+15$ | $3.926 \mathrm{E}+03$ | $9.01 \mathrm{E}+15$ |  |
| 2389 | 2611.83636 | 597.77915 | 1.861446 | $-9.007 \mathrm{E}+15$ | $4.839 \mathrm{E}+15$ | $1.02 \mathrm{E}+16$ |  |
| 2390 | 2612.30961 | 598.66008 | 1.861446 | $2.200 \mathrm{E}+12$ | $4.839 \mathrm{E}+15$ | $4.84 \mathrm{E}+15$ |  |
| 2391 | 2612.78286 | 599.54100 | 1.861446 | $-1.939 \mathrm{E}+12$ | $-1.182 \mathrm{E}+12$ | $2.27 \mathrm{E}+12$ |  |

The comparison of coordinates from the algorithm and coordinates of CAD drawing are summarized in Table 5.

Table 5. Comparison of Coordinates for the Beginning Points of Curves

| Section | Coordinates of Beginning Points |  |  |  |
| :---: | ---: | ---: | ---: | ---: |
|  | CAD |  | Calculated |  |
|  | x | y | x | y |
| Circular Curve 1 | 687.4211 | 71.7278 | 686.9910 | 71.9794 |
| Circular Curve 2 | 1278.7013 | 135.5798 | 1278.3974 | 135.3001 |
| Circular Curve 3 | 1929.9367 | 298.0468 | 1929.5372 | 298.1528 |
| Tangent Section | 2610.1388 | 594.6192 | 2610.4166 | 595.1364 |

The comparisons of radii of curves, lengths of curves, and central angles are shown in Table 6.

Table 6. The Comparison of $R, S, \Theta$ for the reverse curve

| Section | Radius of Curve(R) |  | Length of Curve(S) |  | Central Angle( $\Theta$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | CAD | Calculated | CAD | Calculated | CAD | Calculated |
| Curve 1 | 500 | 500 | 636.91 | 637.00 | 73.0 | 73.0 |
| Curve 2 | 700 | 700 | 700.00 | 700.00 | 58.0 | 57.3 |
| Curve 3 | 600 | 600 | 800.00 | 801.00 | 77.0 | 76.5 |

When Table 5 and 6 are compared, the horizontal alignment analysis algorithm is applicable for the simple curves and clothoid curves.

## 4. CONCLUSION

In this research, the horizontal alignment analysis algorithm was developed which can recognize the highway sections whether they are tangent sections or curve sections using the real world coordinate data. The proposed algorithm for horizontal curve analysis includes the identification of beginning and ending points of horizontal curves for the circular and transition curves, the parameter of clothoid, radius of circular curve, and length of circular and transition curves. The calculated coordinates for the beginning of curve, beginning of tangency, values for the radius, length of curve, clothoid parameter, and central angle show almost similar to the real world coordinates and real world values. The identification algorithm of horizontal curves expects to be used as a basis of automatic procedure which can identify the highway deficient sections along the highway route and analyze highway safety in terms of quantitative measures.

## References

Hickerson, T.(1964) Route Location and Design, McGraw-Hill
Yun, DukGeun and Sung, JungGon(2004) Development of theoretical horizontal alignment algorithm using highway coordinates. The $6^{\text {th }}$ KSRE Conference Proceeding, Korean
Society of Road Engineers, Oct. 2004
TAC(1999), Geometric Design Guide for Canadian Roads, Transportation Association of Canada

